

Objective



Wabiskaw-McMurray

Determine the vertical and lateral isolation within the currently defined Hardy Wabiskaw-McMurray A Pool, using pressure data and integrated engineering techniques.

Pressure

The Board's view (Decision 2004-045 for Hardy):

“The Board acknowledges that there are significant limitations to the use of pressure data in determining gas pooling in the areas under consideration. These limitations are due to:

1. both the quantity and quality of the pressure data, including the lack of historical pressure data,
2. commingling of production and pressure measurements from different stratigraphic intervals,
3. insufficient shut-in times and,
4. in some cases, the use of surface pressures.

The Board found very few cases where the pressure data were sufficiently definitive to base pooling decisions upon. In most cases, the Board relied more on geological data than on pressure data.”

Geology

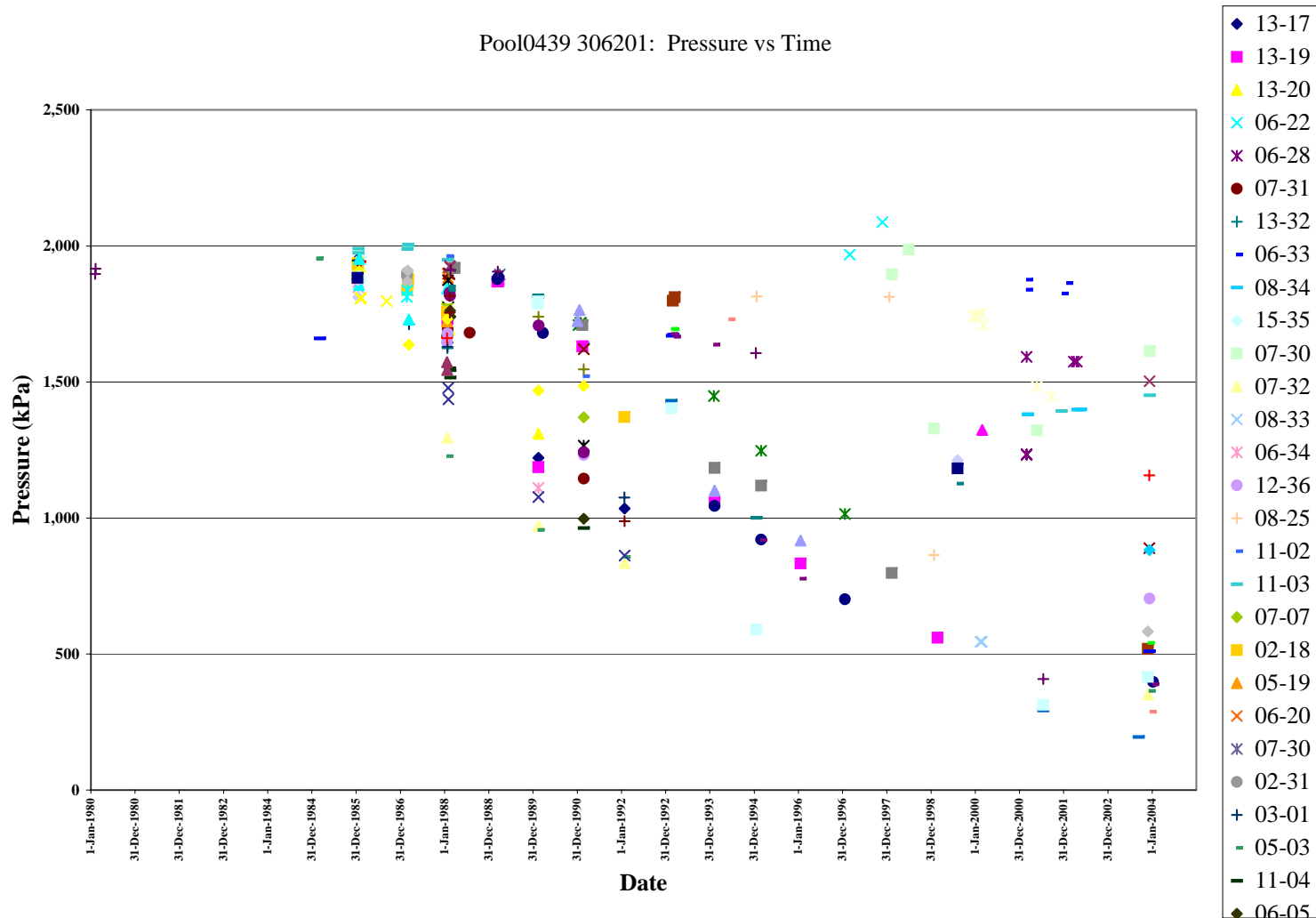
“However, I do not believe that the questions of pressure communication amongst lithologic units or between gas and bitumen zones can be answered definitively by stratigraphic analysis and mapping alone.” (RGS '03)

Pressures for Wabiskaw-McMurray A Pool (SSG CD)



Wabiskaw-McMurray

Pool0439 306201: Pressure vs Time





Wabiskaw-McMurray

Methodology

Diagnostic Techniques to define ROI

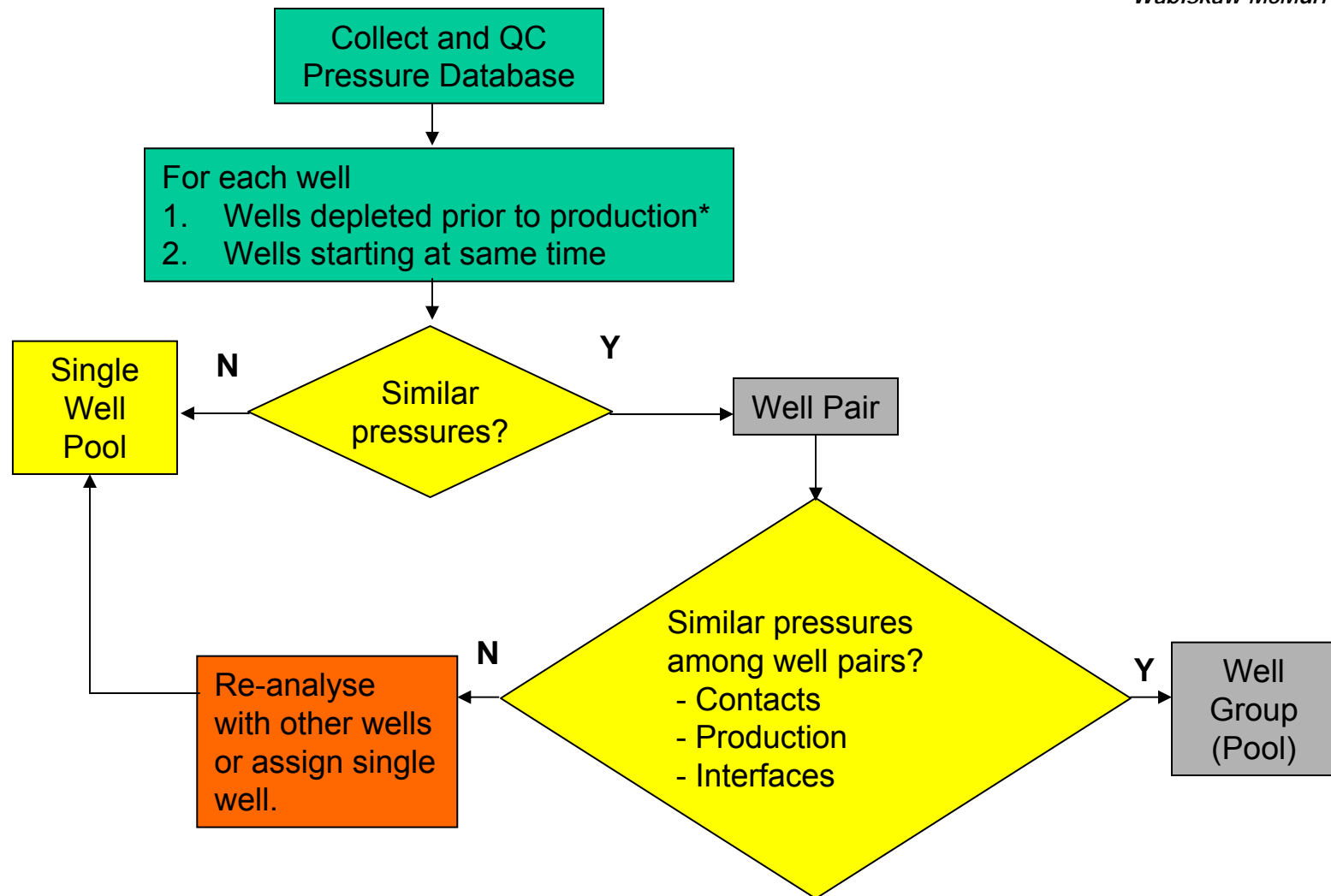


Wabiskaw-McMurray

- Pressure versus time - Examined long term reservoir pressure trends.
- Production Decline - Wells in pool should decline on same decline trend due to consistent pressure drop within high permeability pool. Pools with different pressure declines will decline at different rates.
- Gas–Oil or Gas-Water Contact Differences - Similar contact within pool implies continuity / differences imply discontinuity.
- Seismic bright spots - Indicate where gas is and is not areally. Used where seismic coverage and resolution was available.
- Material Balance (P/Z vs. Gp) - Estimate gas in place. Useful to compare to volumetrics and determine if boundaries reasonable.
- Stratigraphic correlation - Correlates lithological units between wells, however it does not define hydraulic communication.
- Structural mapping - Useful to define pool boundaries. Well control may be sparse

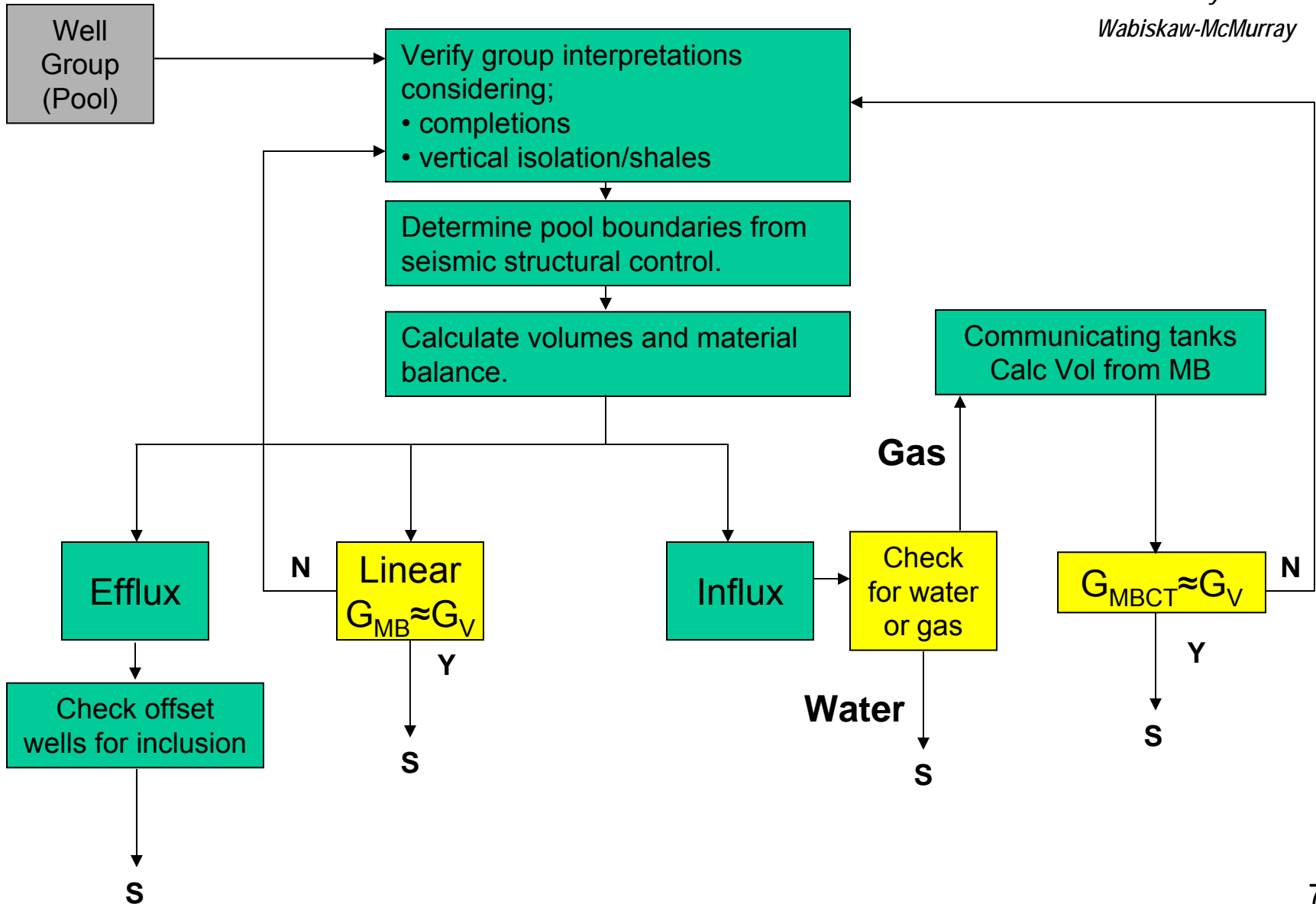
Determined 25 Areal Pools & 48 vertically and laterally isolated pools

Determining Regions of Influence – Determining Well Groups



* Depleted wells must have pairs unless initial pressure incorrect

Determining Regions of Influence – Determining Pool Boundaries Size



Admissibility of Pressures

Interpretation, Data

Comments on Pressure

Review of 75 well tests

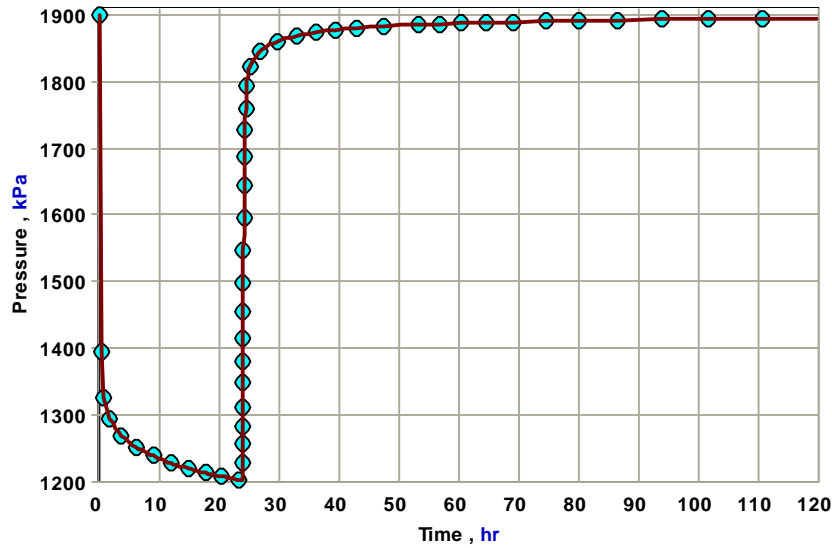
- The data quality is sufficient to accurately extrapolate the reservoir pressure and determine the reservoir flow characteristics. In most cases it is reasonable to expect a data accuracy within +/- 40 kPa.
- The accepted test procedure during field development was a 4 point test followed by a 12 hour flow and a 24 hour buildup. Later tests (1993 onwards) typically had 36 hour flow times and 10 days of buildup time.
- Pressure transient analysis shows the average permeability is in the order of 500 mD. The average skin effect ranges from +2 to +15. Higher skin values are due to turbulent flow (low pressure and high velocity).
- Initial reservoir pressures vary between 1800 and 2000 kPa. The low pressure promotes high gas compressibility.
- Due to the combination of high formation permeability, high gas compressibility and the relatively short flow times, the pressure transients are characterized by radial flow. An accurate extrapolation of a semilog (Horner Plot) is possible to obtain the reservoir pressure.

- 20 Years of data
- Over 300 points
- Good quality data (little surface data)

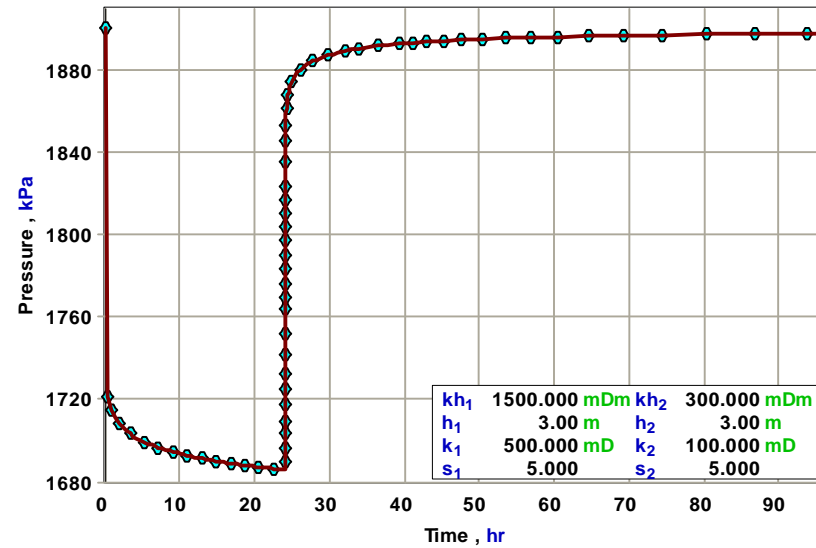
Synthetic Buildup Response



Wabiskaw-McMurray



Single layer (100 md)

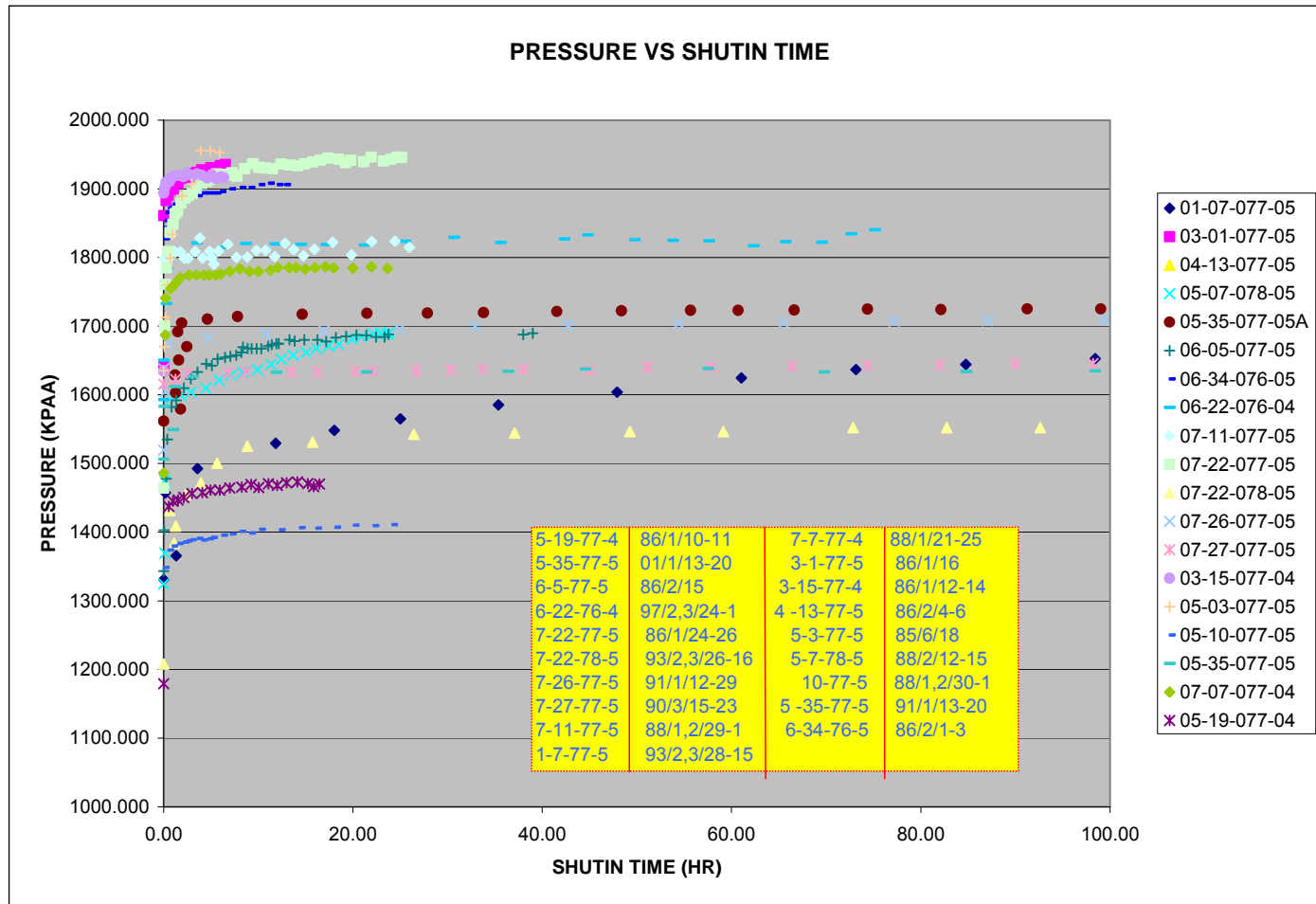


Dual Layer (100/500 md)

Actual Field Buildup Response



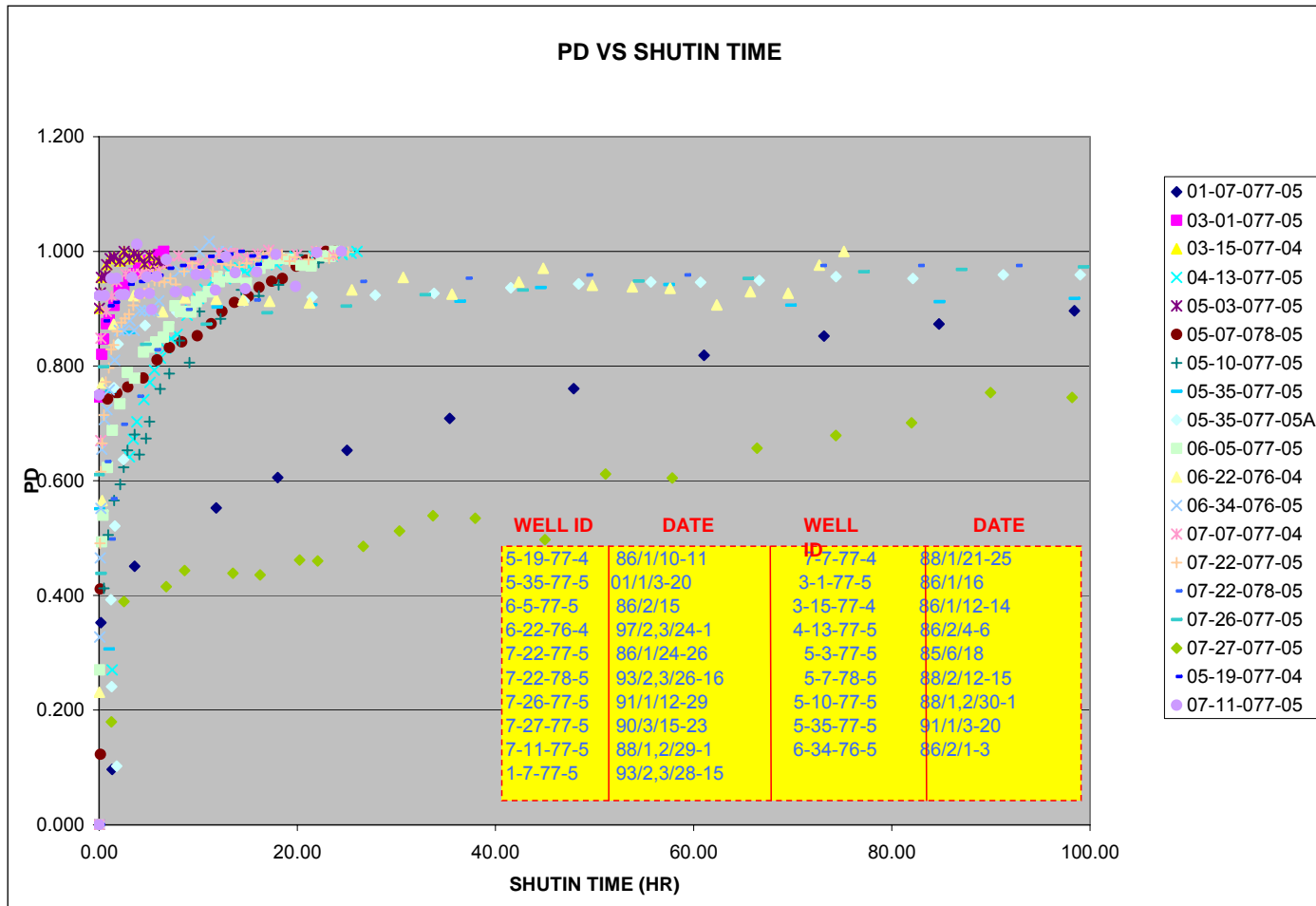
Wabiskaw-McMurray



Actual Field Buildup Response - Dimensionalized

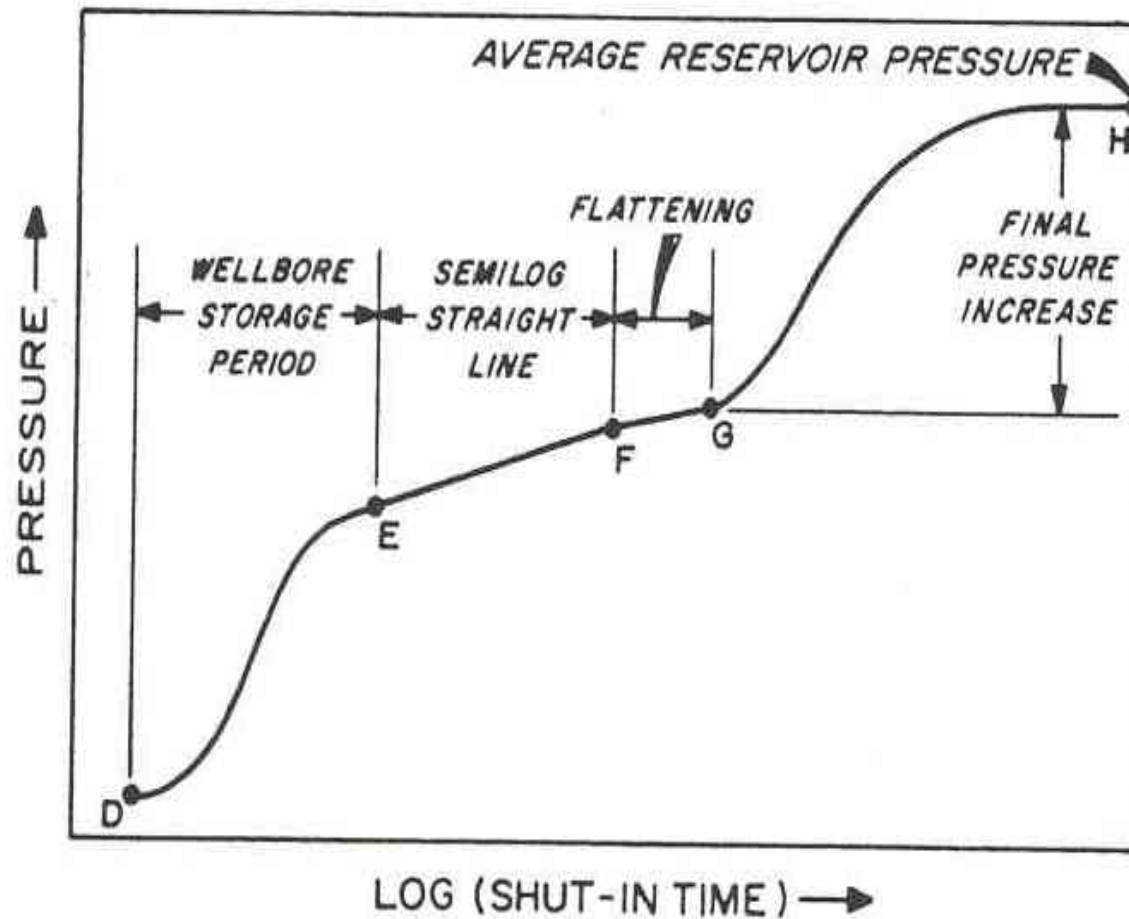


Wabiskaw-McMurray

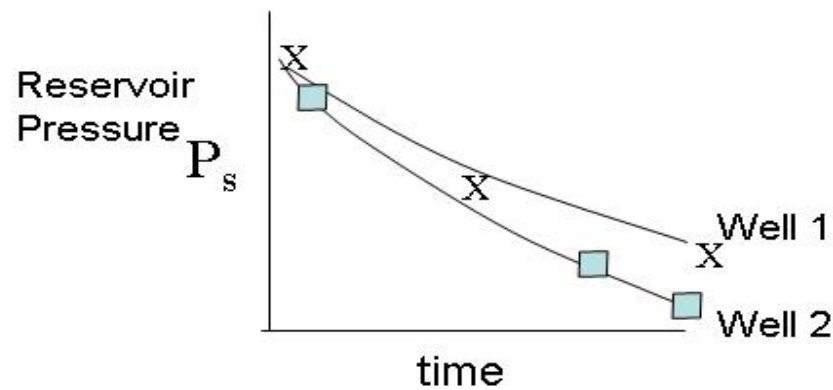


$$P_d = \frac{P - P_{\min}}{P_{\max} - P_{\min}}$$

Pressure Build-Up Response for Single Well, Dual Layer Bounded Reservoir



Pressure behavior of Laterally Isolated Reservoirs

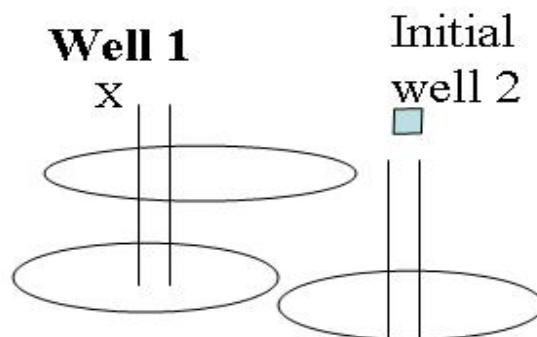


Divergent Behavior
Pressure difference as measured by wells show differences in pressure



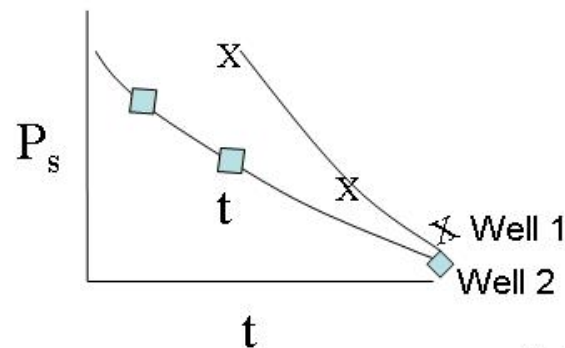
drain two pools

(Well 1 and well 2 drain separate compartments)

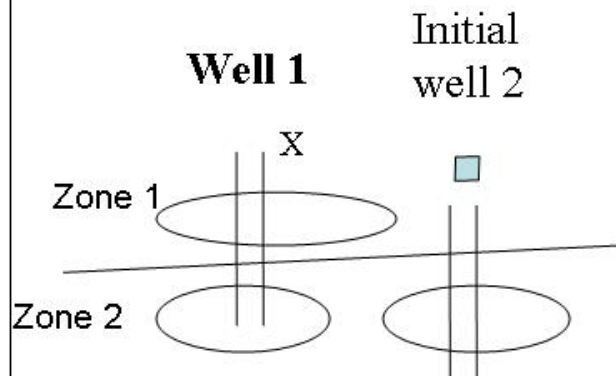


Cross Sectional view

Pressure Behavior of Commingled Reservoirs

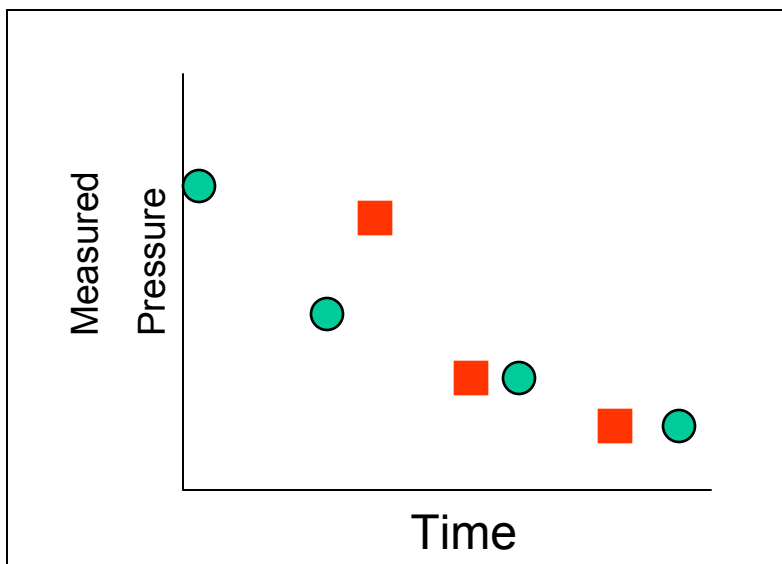
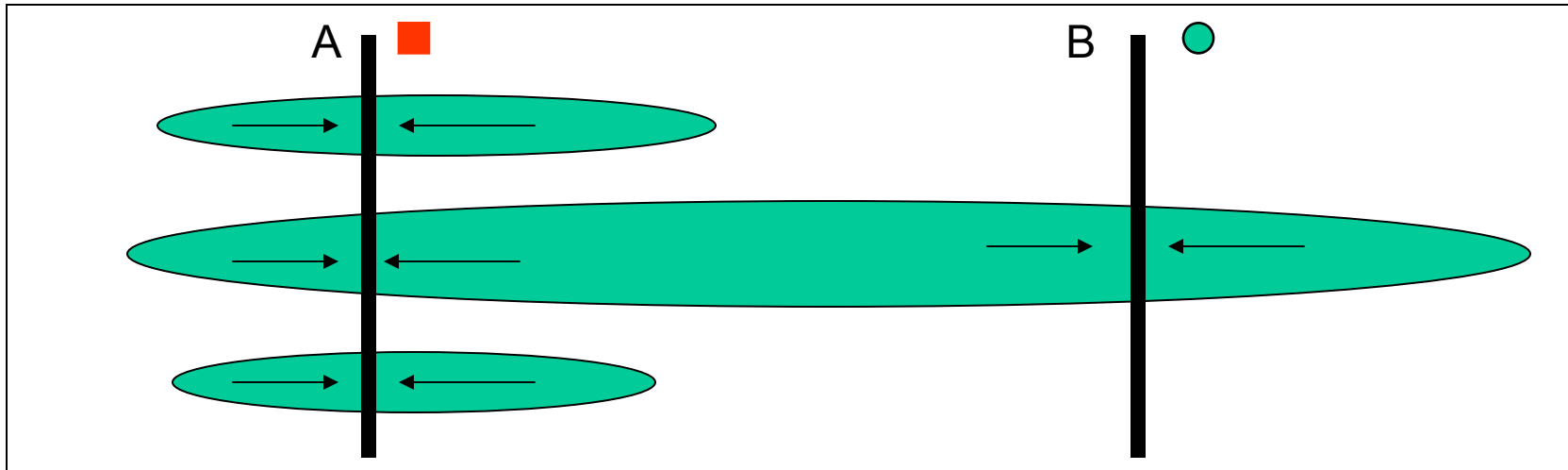


Convergent
behavior



Initial measured pressure is different in later drilled wells because one zone is vertical hydraulically isolated from the other zone; Zone 1, has higher initial pressure than the current pressure in Zone 2, the more continuous zone. However, with crossflow and production measured pressure in both zones will eventually be the same.

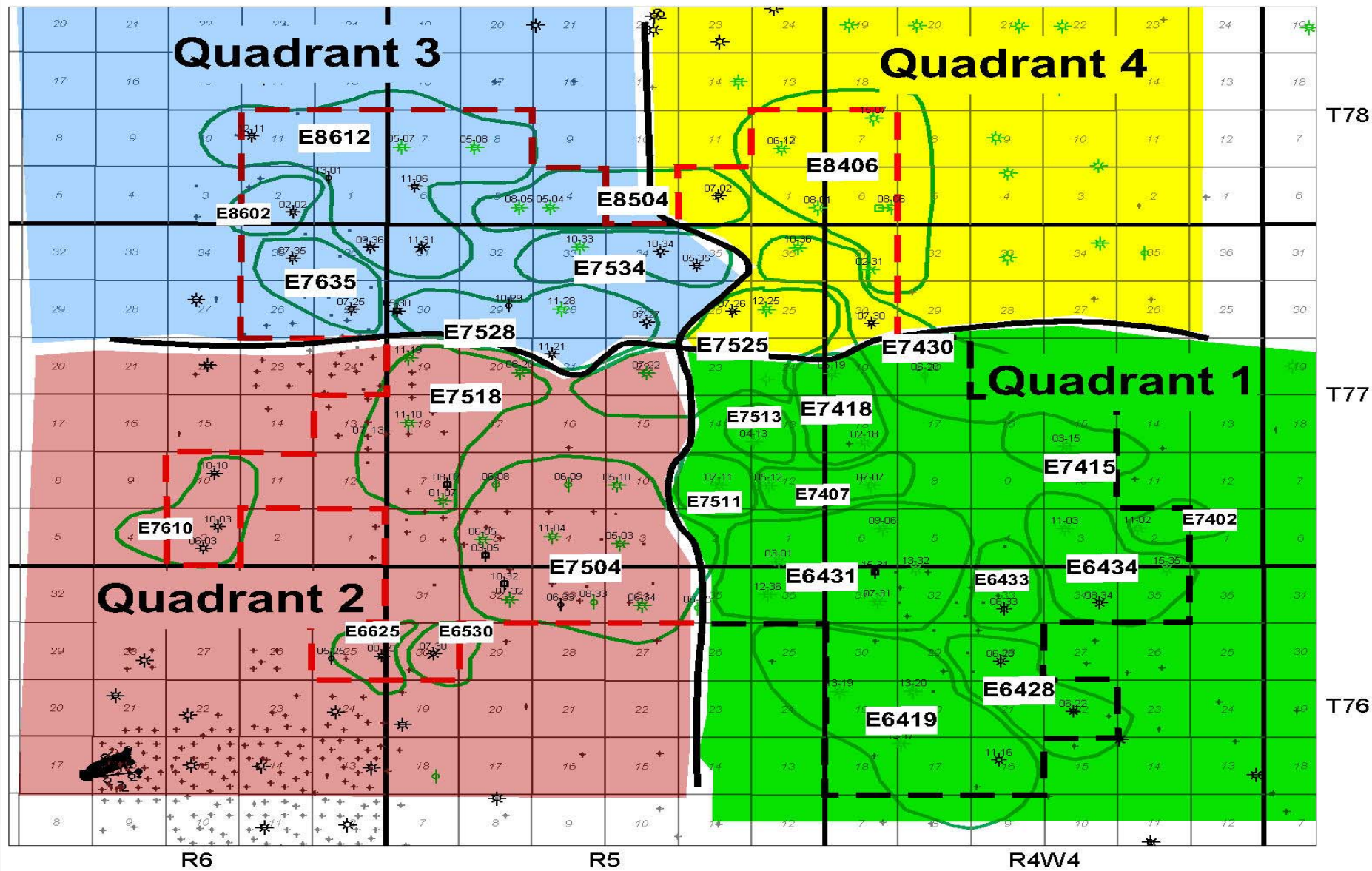
Explaining Pressures in Hardy Field



- Permeability of formation is very high $K \sim 500$ md (average PTA)
- Large Δp contrast not expected layer equalize $(kh \Delta p)_1$, $(kh \Delta p)_2$
- Even though multiple completions often one zone dominant

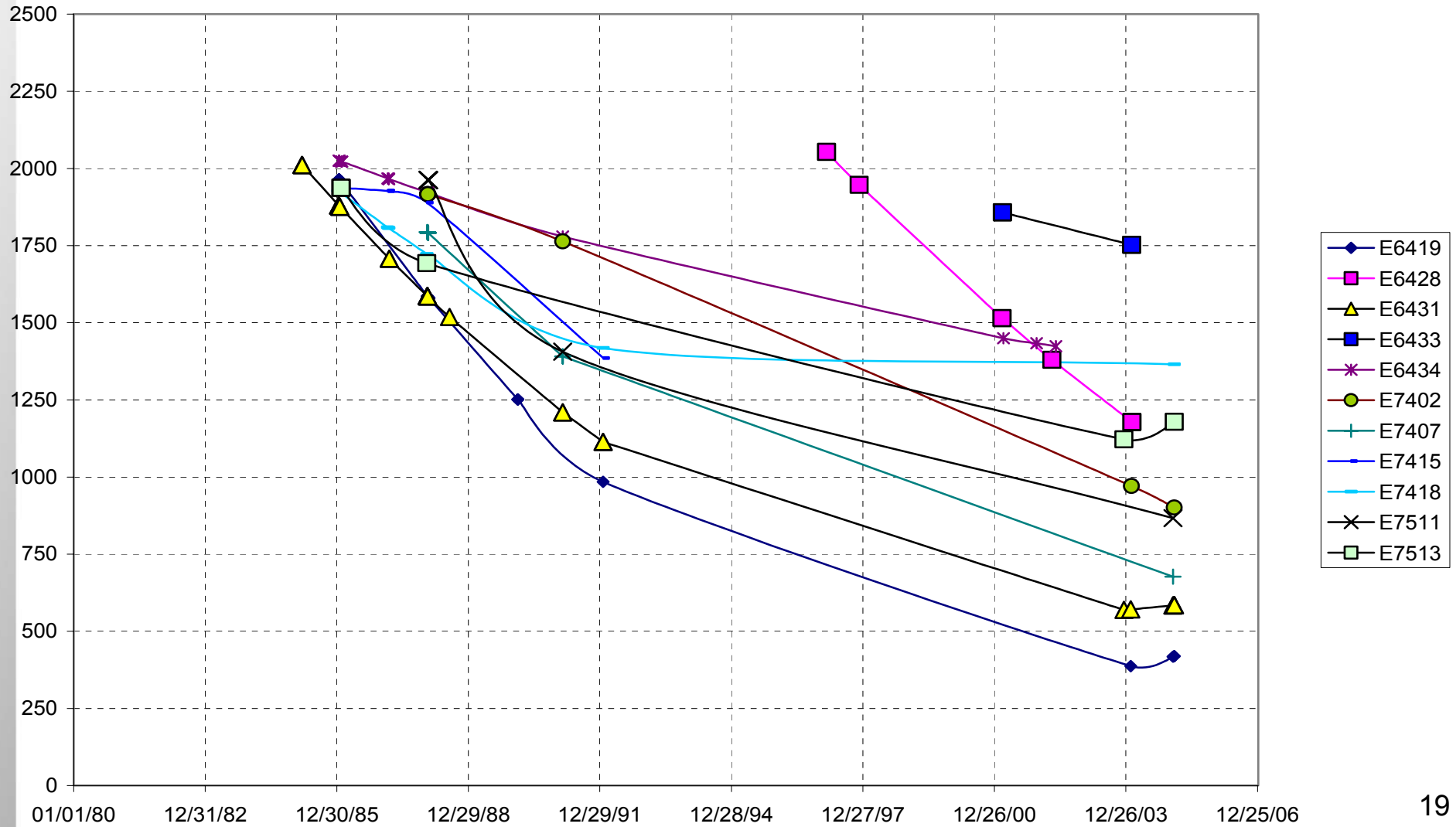
Actual Field Pressure vs Time

Pool Pressure Trend Quadrants



Quadrant 1

Quadrant 1

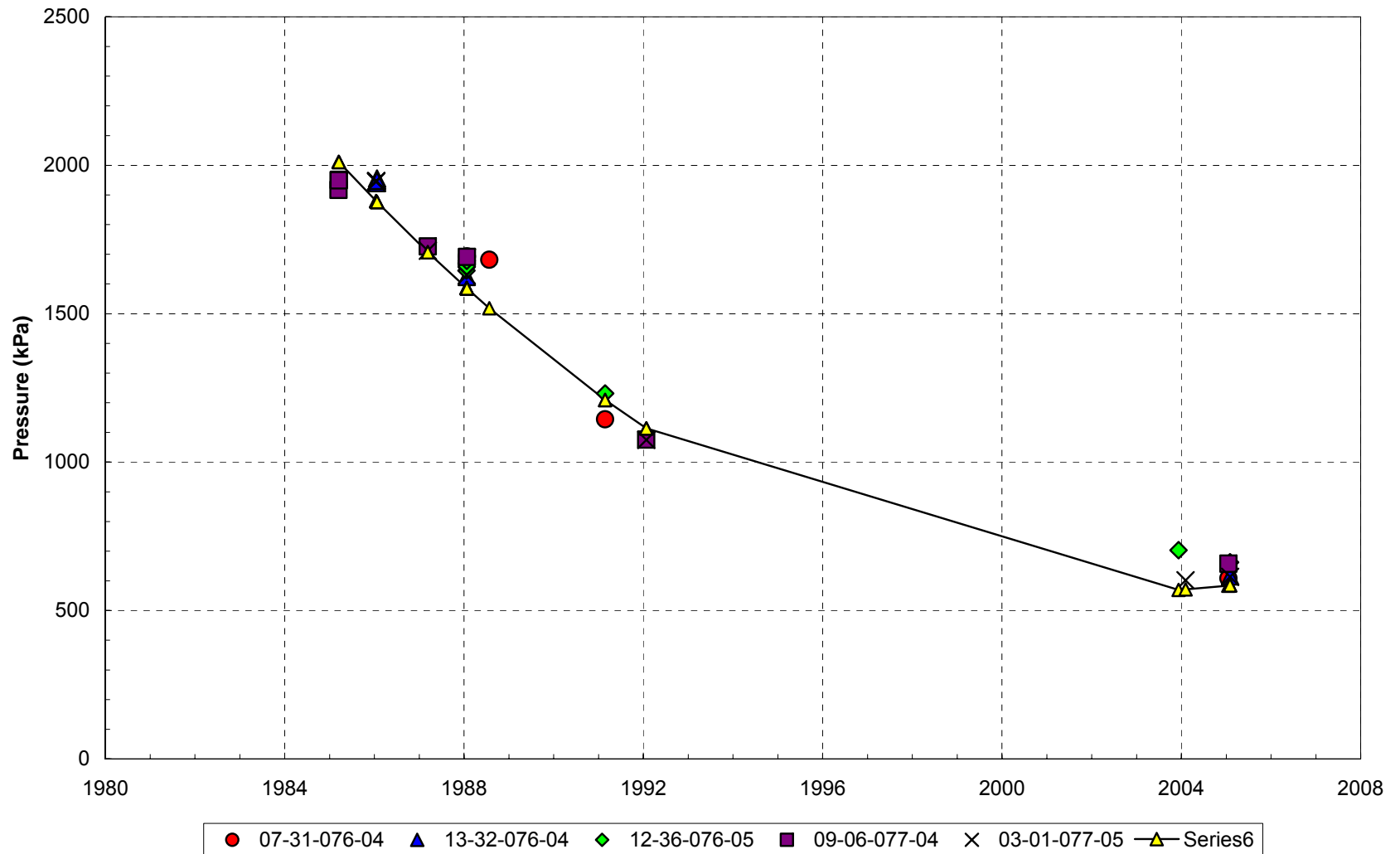


An Example of Trendlines Plotted - E6431



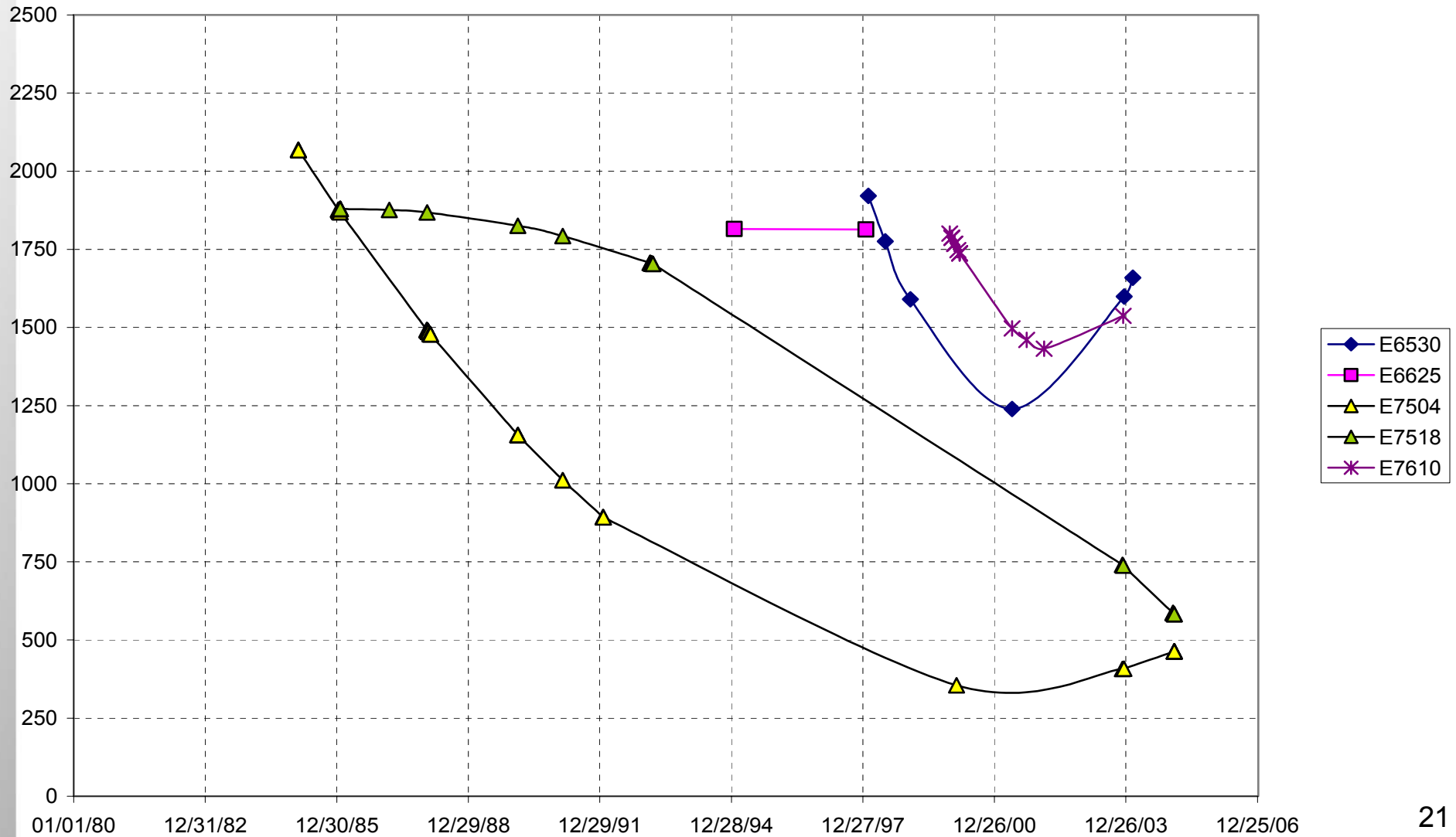
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E6431



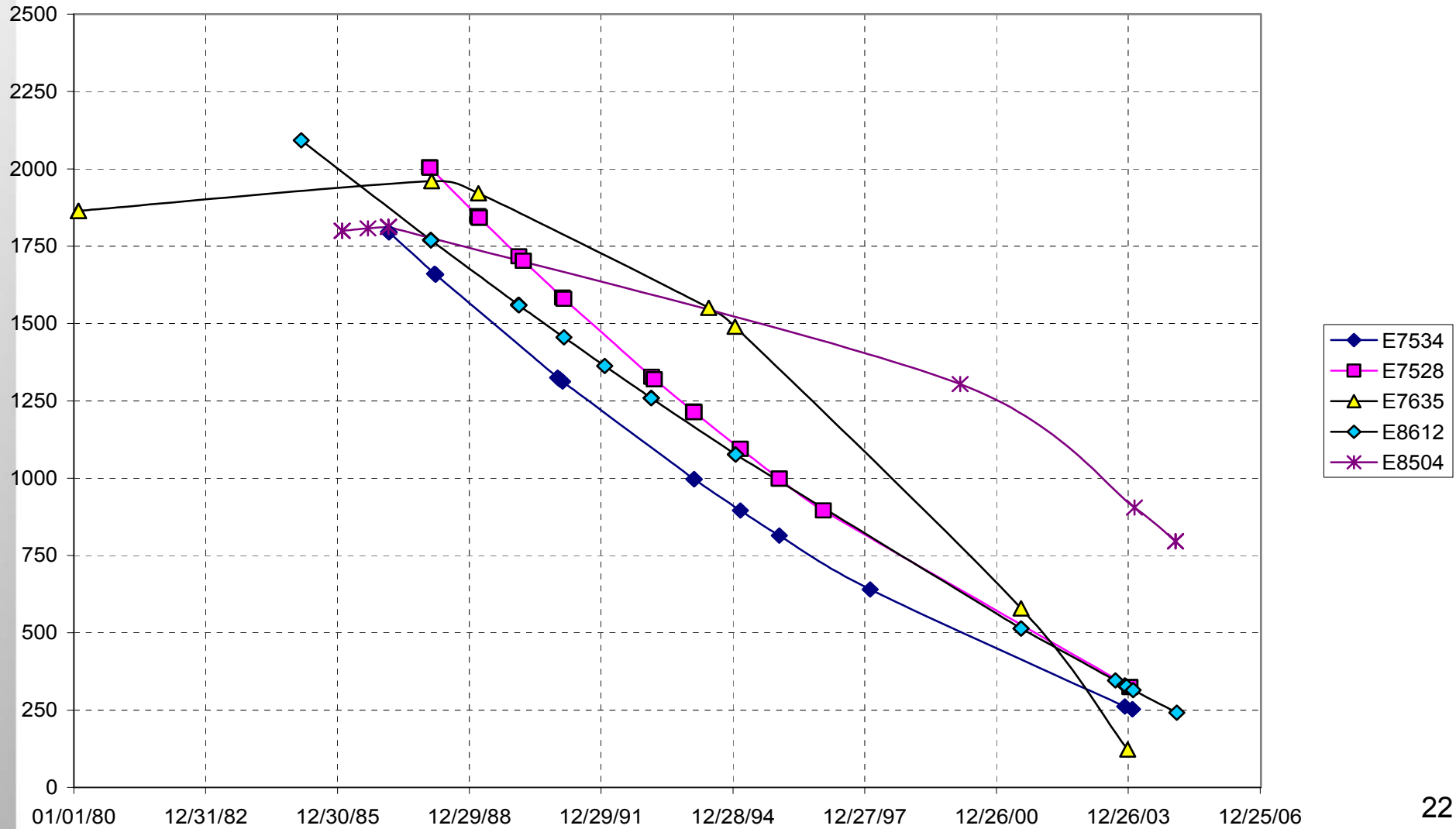
Quadrant 2

Quadrant 2



Quadrant 3

Quadrant 3

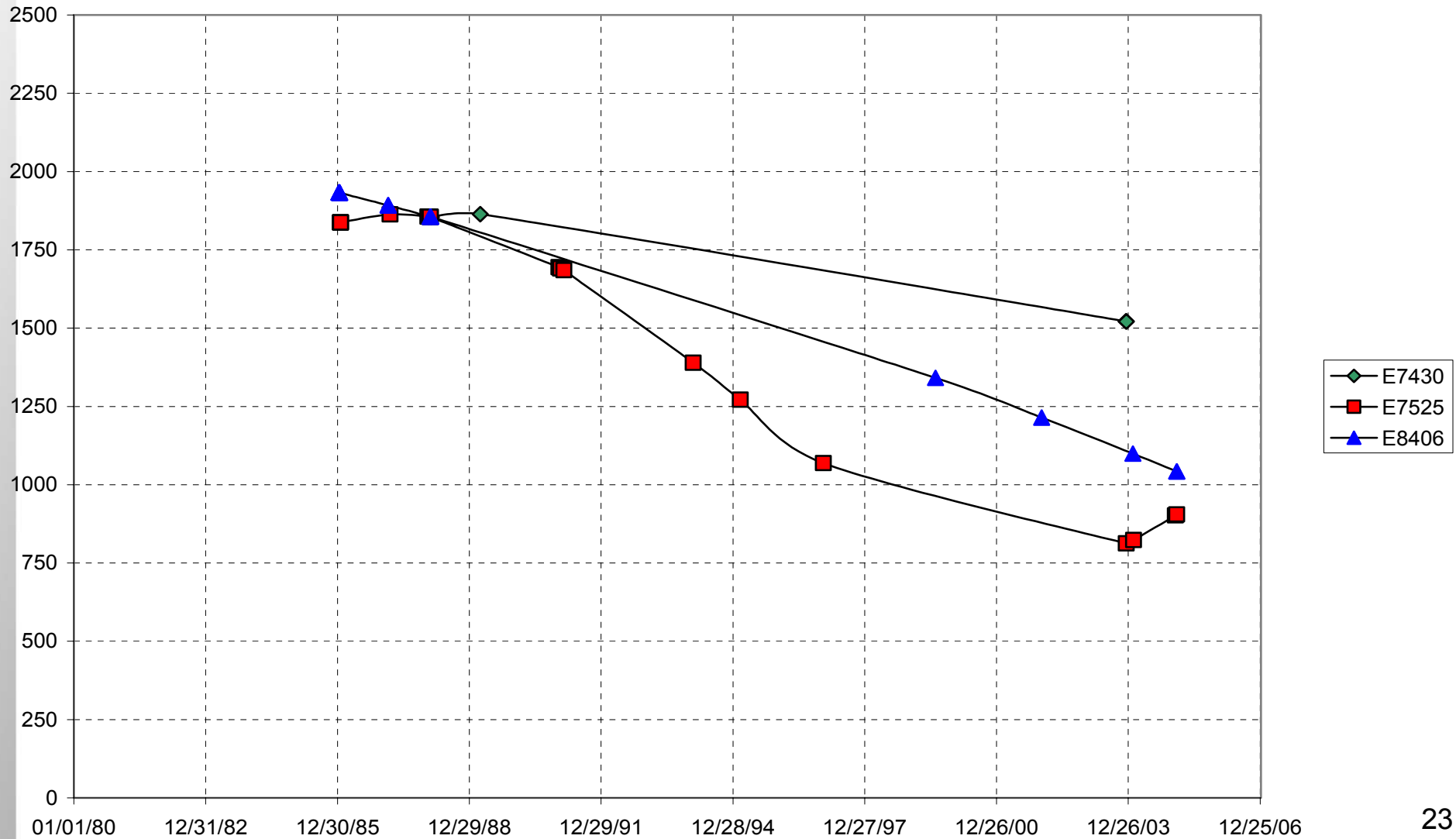


Quadrant 4

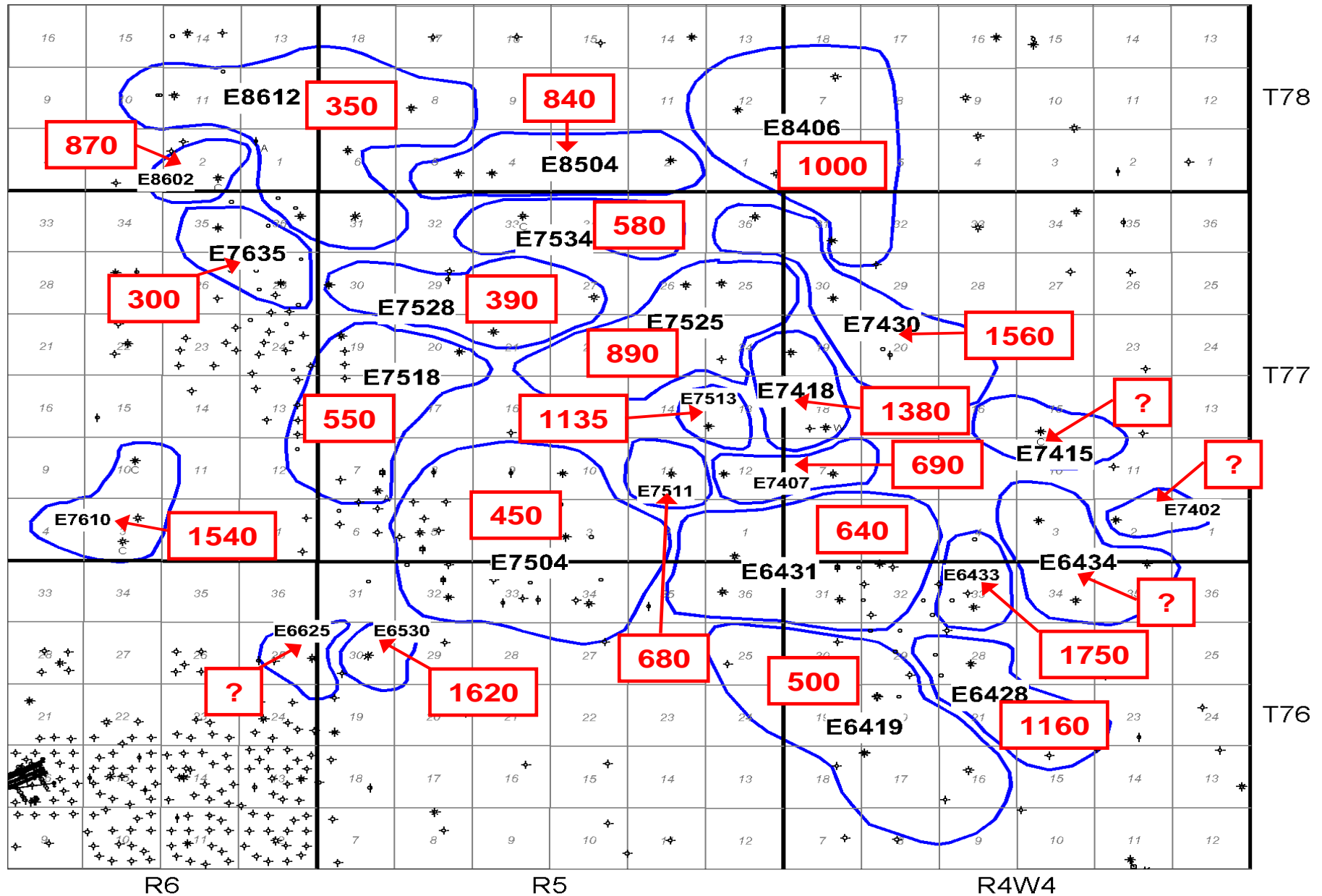


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Quadrant 4

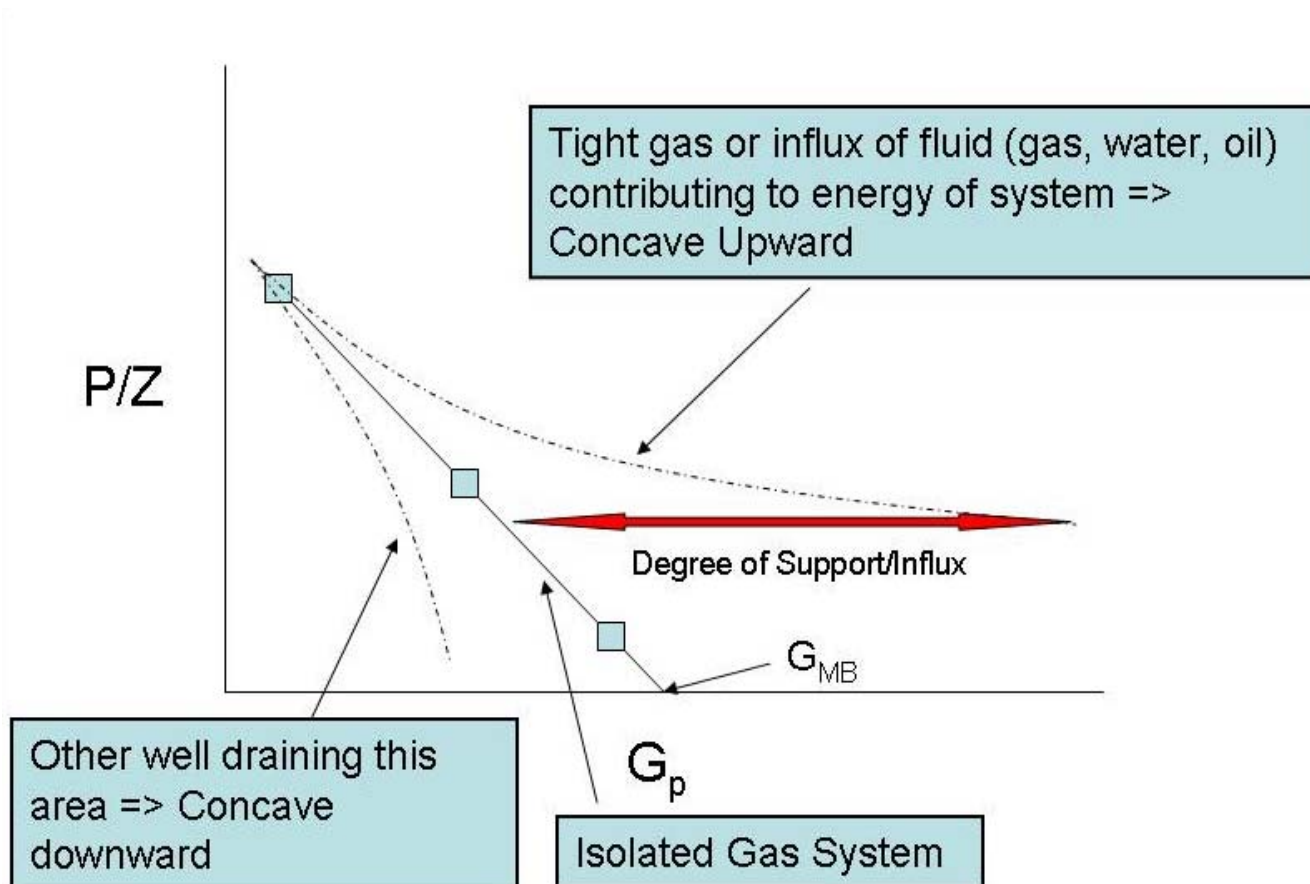


Current 2004/2005 Pool Pressures

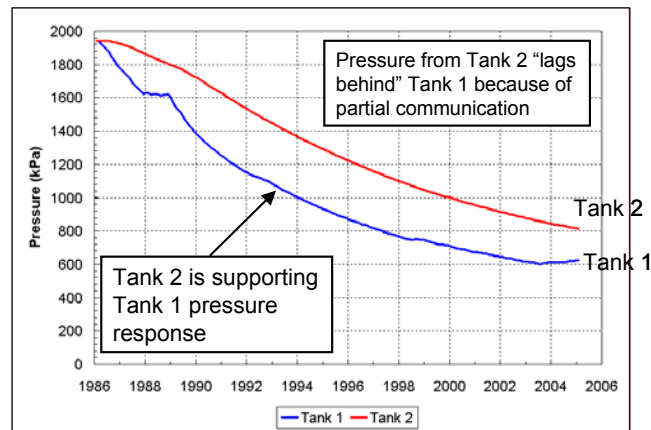
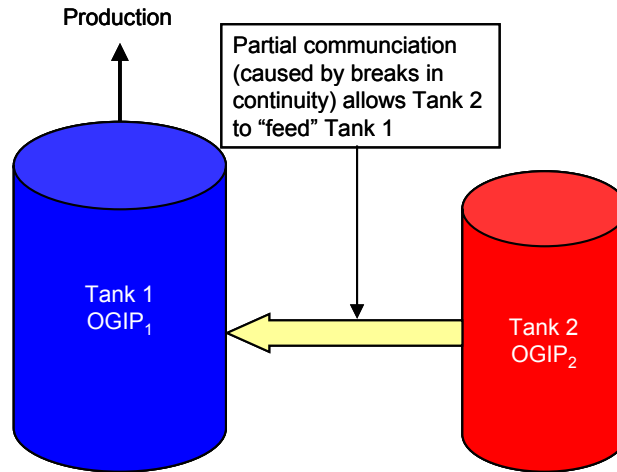


Pressure/Z vs Gas

Material Balance P/Z vs. G_p Scenario Schematic



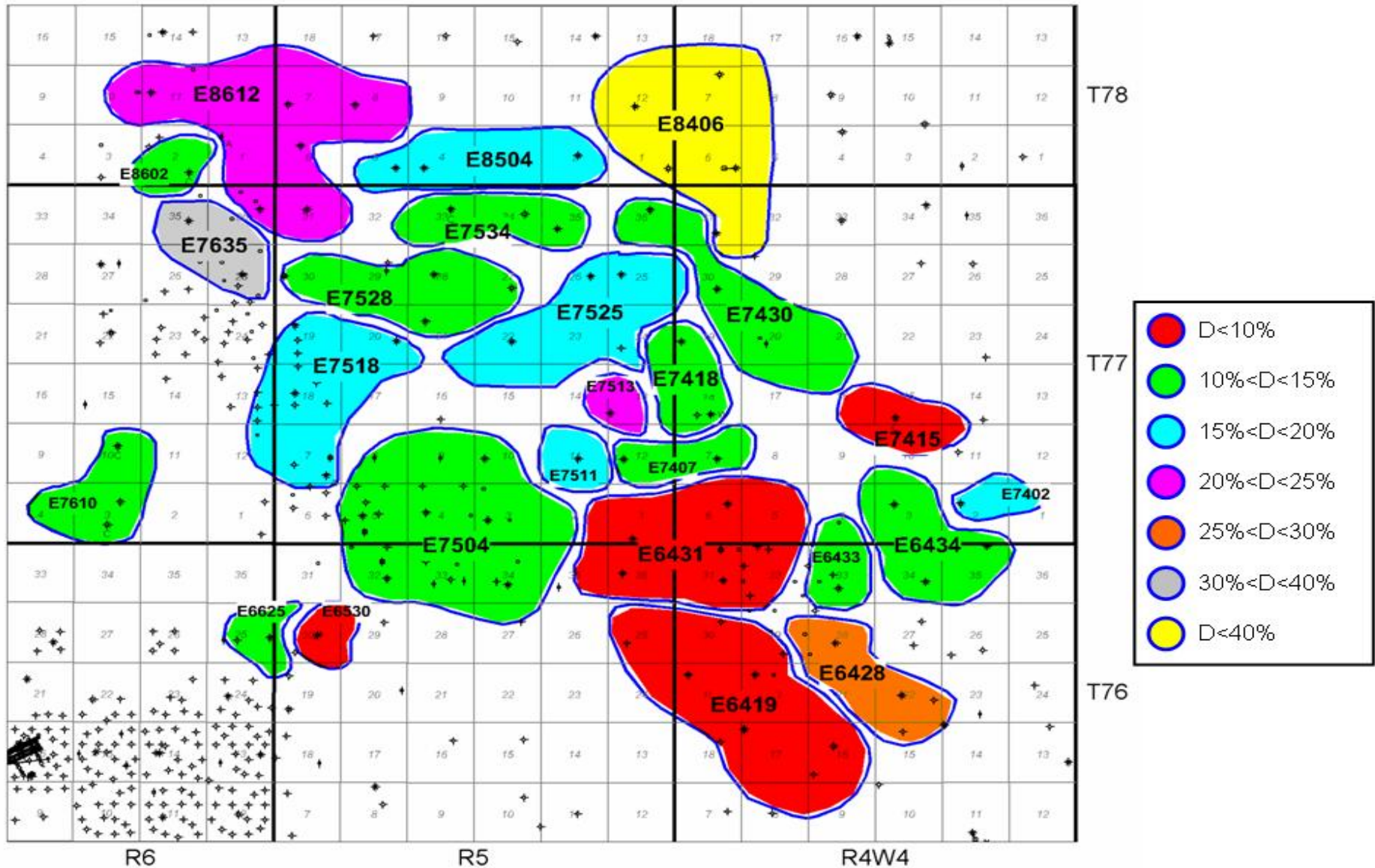
Communicating Tanks Model



Used in 4 of 25 pools

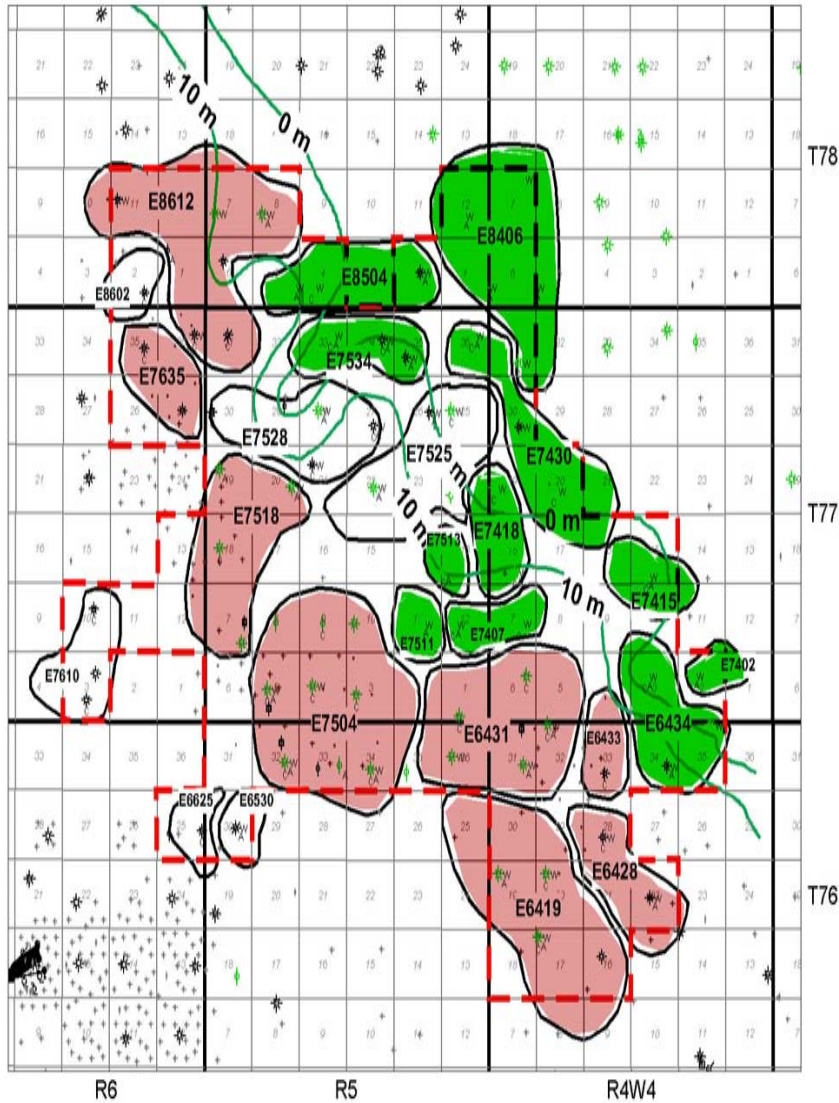
Production Decline

Areal View of Pool Decline Rates

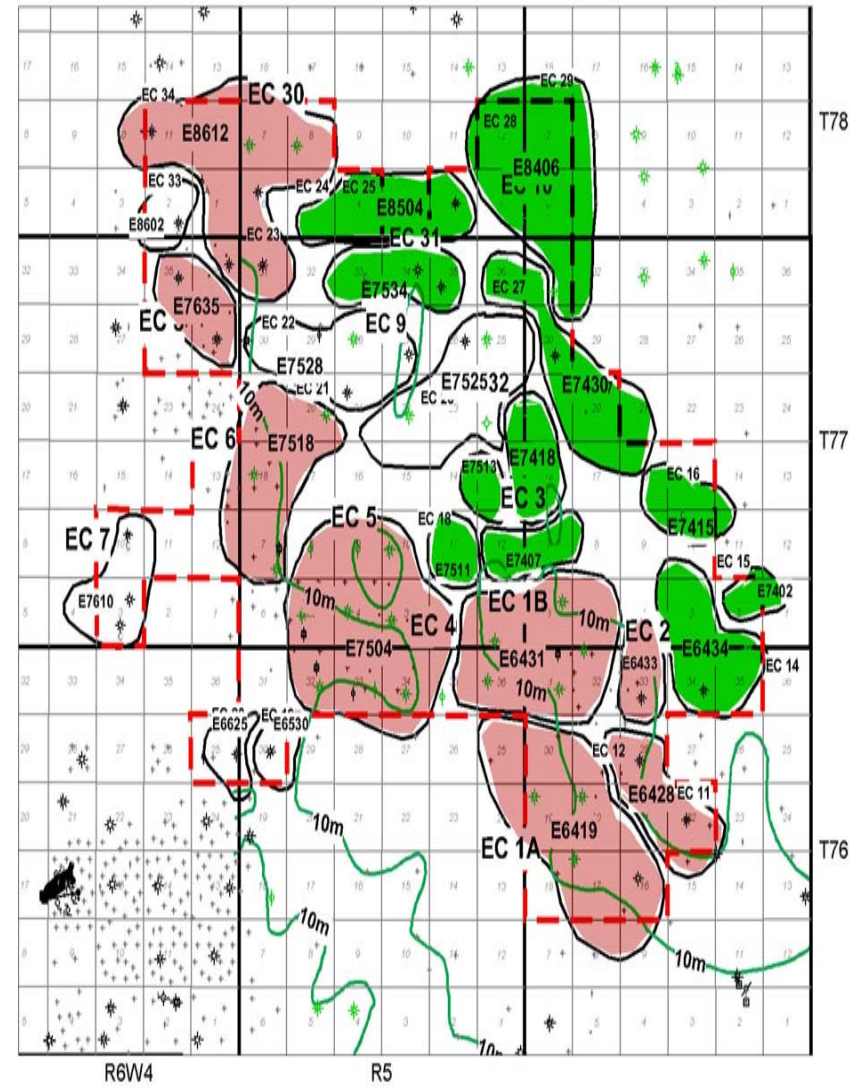


Suitability for Thermal Development

Potentially Recoverable Bitumen



RGS



Petrel Robertson

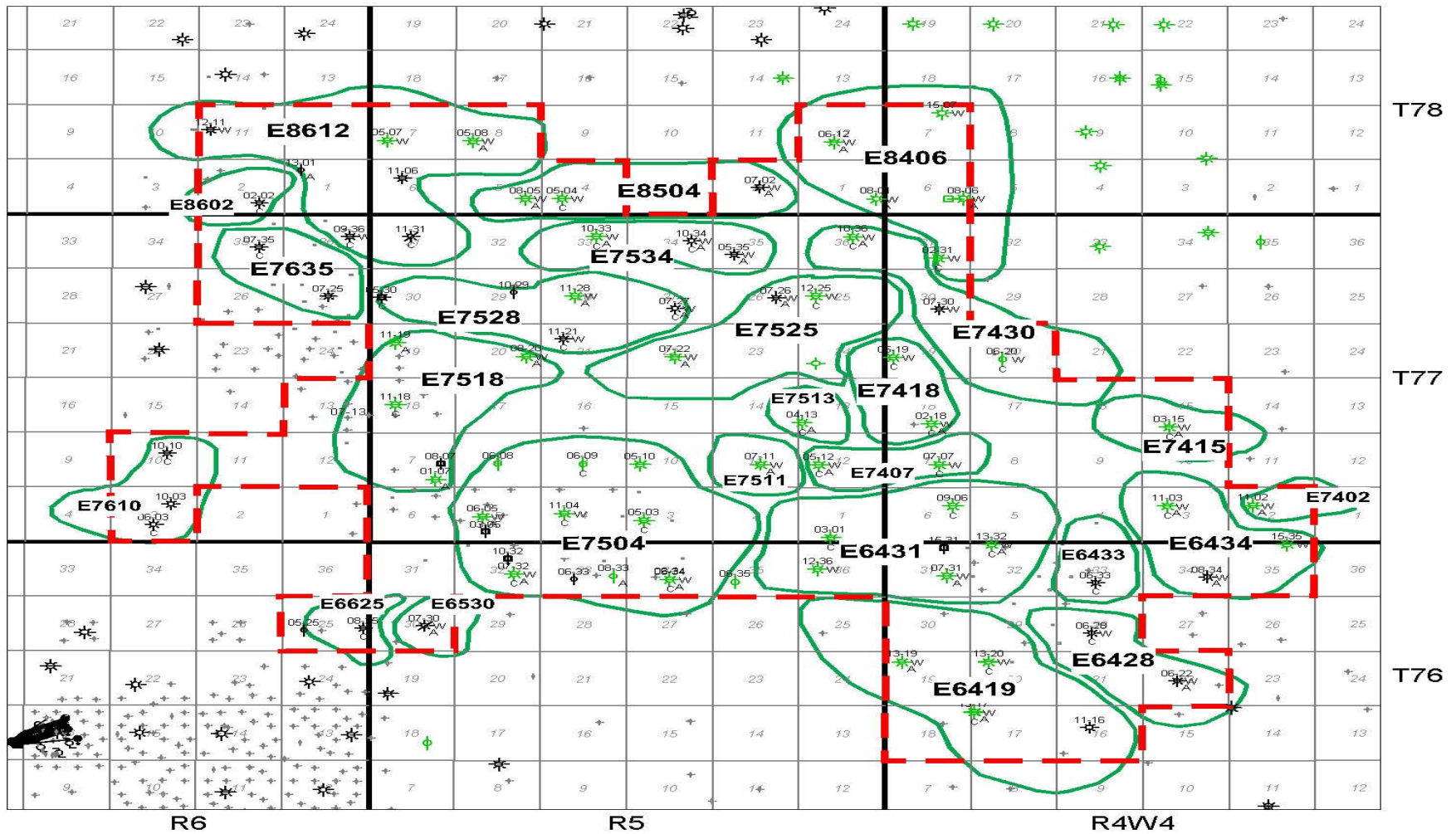
SUMMARY



Wabiskaw-McMurray

- There is sufficient usable pressure data to make pooling decisions
- The pressure behavior within each smaller pool shows little difference within the pool, but distinct differences between other smaller pools;
- Analysis is based on an integration of pressure, production, geological and geophysical data;
- Disconnects (compartmentalization) in pool continuity supported by pressure and production decline differences, contact differences and seismic breaks;
- Smaller pools can be defined in the current Hardy Wabiskaw-McMurray A Pool resulting in revised ROI's

Gas Pools in Hardy as determined by EPIC Consulting Services Ltd.



SCENARIOS



Wabiskaw-McMurray

- Case 1 – Non-associated gas - Wabiskaw C where the Wabiskaw D is present and sealing, or McMurray gas where there is no underlying McMurray bitumen (produce).
- Case 2 – Associated gas - McMurray where there is insufficient bitumen (<10m), or Wabiskaw C gas where the regional Wabiskaw D shale is missing (produce).
- Case 3 – Associated gas (McMurray or Wabiskaw C gas where the regional Wabiskaw d shale is missing) where there is sufficient bitumen (>10m) but is not viable according to the GIAG Thermal Sub-Committee recommendations (produce)
- Case 4 – Associated gas (McMurray or Wabiskaw C gas where the regional Wabiskaw d shale is missing) where there is sufficient bitumen (>10m) to be viable according to the GIAG Thermal Sub-Committee recommendations. PEOC's modelling work shows that SAGD recovery is insensitive to top gas pressure, and therefore these wells should also be allowed to produce.